

Part III
Attachment III-E
Appendix III-E.4

**SUMMARY OF HYDROGEOLOGIC TESTING IN SELECTED
PIEZOMETERS**

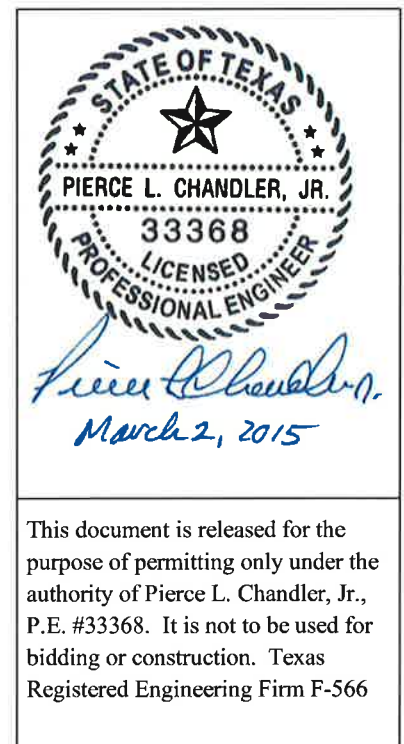
Pescadito Environmental Resource Center
MSW No. 2374
Webb County, Texas

PESCADITO
ENVIRONMENTAL RESOURCE CENTER

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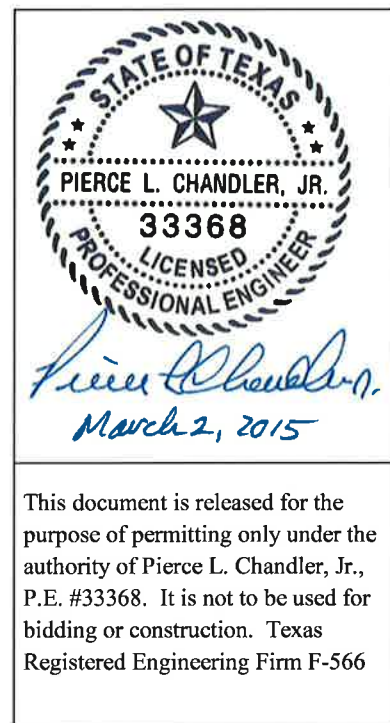
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1.0 INTRODUCTION

Hydrogeologic testing was conducted in ten piezometers installed as part of the Phase III site investigation at the Pescadito Environmental Resource Center (PERC) site. Phase III piezometers were installed in what appeared to be potentially transmissive zones, i.e., isolated sandy and/or silty intervals in the predominantly clay matrix based on the evaluation of previous Phase I, II, and III boring logs and geophysical data. Information on the piezometer installations can be found in Appendix III-E.2, *Subsurface Investigation Report*.

The hydrogeologic tests included falling head and rising head tests induced by inserting and removing solid slugs (i.e., slug tests). Based on the results of the slug tests, a subset of five piezometers indicating the highest transmissive potential were selected to conduct higher-stress, single-well, pump-down tests.

2.0 SLUG TESTS

Slug tests were conducted on ten piezometers (B-11A, B-101, B-102, B-106, B109A, B-114A, B-115, B-118, B-124, and B-126) located within the footprint of the proposed facility in Webb County, Texas. The slug tests were conducted between January 12, 2012 and January 22, 2012.

Each slug test consisted of one falling head test followed by one rising head test. To confirm repeatability of the results, multiple slug tests were conducted at each piezometer and various slug sizes were employed during each slug test. The slug test procedures and results are summarized in Table 1 attached.

2.1 Setup

Prior to conducting each slug test, a pressure transducer was programmed using a laptop computer. The date, time, site information, and logging instructions were programmed. The logging instructions consisted of recording the date, actual time, elapsed time, barometric pressure, water pressure, and the level of the water column over the pressure transducer (in feet).

In addition, the sample frequency/schedule of the transducer was configured to record data at one-second intervals. The piezometer construction details, static water elevation in the piezometer, and the length of the slug were used to determine the position of the transducer in the piezometer for each slug test. The pressure transducer was placed in the piezometer between four to five feet below the approximate elevation of the bottom of the slug. The transducer cable was secured at the top of the piezometer so that the pressure transducer level in the piezometer was not altered during the test. Any transducer cable extruding out of the piezometer was placed away from areas of walking or vehicle traffic.

The static water level in the piezometer was measured with both the pressure transducer and a water level meter to confirm the transducer was functioning properly. In addition, the hydrostatic pressure at the transducer elevation was calculated and compared to the pressure measured by the transducer.

2.2 Falling Head Test and Rising Head Test

Once it was confirmed that the transducer was functioning properly, the slug was lowered into the piezometer in a quick and controlled manner as to prevent creating large disturbances in the

water level. The increasing head of the water column was monitored by the field personnel with a laptop computer. Once the maximum displacement was observed, the line suspending the slug was secured to the top of the piezometer. The transducer recorded the falling head of the water column for the rest of the falling head test.

The slug was removed completely out of the water column and piezometer in a quick and controlled manner to begin the rising head test.

Information on slug dimensions (length and displacement volume) and corresponding test duration for each test are included in Table 1.

2.3 Slug Test Data Evaluation and Results

All slug test data was first evaluated by reviewing the time-drawdown data to verify transducer function, etc. For actual analysis, the normalized falling and rising head data (i.e., instantaneous displacement divided by initial displacement or ht/H_i) with respect to time was plotted for each test. Normalized time-drawdown offers additional advantages as well:

- Allows head-to-head comparison between tests run with different slug displacements, etc., in the same piezometer;
- Allows head-to-head comparison between rising head and falling head tests run in the same piezometer, etc.;
- Assists in evaluating piezometer installation quality by comparing repeatability of results from multiple tests; and
- Assists in data validation, e.g., test repeatability, “data signature” appropriate for analysis, etc.

The normalized head data was analyzed using AQTESOLV™ software. During the pre-analysis processing phase of the data evaluation, it was determined that the rising head/falling normalized head responses from all of the slug tests performed on piezometer B-124 were unusable due to a malfunction of the transducer. This data was omitted from further hydrogeologic evaluation.

Hydraulic conductivity was determined for each falling head and rising head test using the Bouwer-Rice method and the Hvorslev method. Much of the time-drawdown data exhibited “double straight-line” signatures (Bouwer & Rice, 1989). In these instances, the later time data (second straight line) was favored for Bouwer & Rice and Hvorslev analyses because it typically represents formation characteristics. Early time data typically represents filter pack characteristics, etc. The time-drawdown data from slug tests performed on piezometers B-101, B-102, B-106, B-114A, B-118, and B-126 indicated a concave up response in the later part of the time-drawdown plots. The concave-upward curving signatures implied storage effects were present and analysis by Bouwer-Rice and/or Hvorslev methods would be questionable. Accordingly, the Cooper, Bredehoeft & Papadopoulos (Cooper, *et al*, 1967) [or Papadopoulos, Bredehoeft, and Cooper Method (1973)] method was also used to determine transmissivity, storativity (estimation), and hydraulic conductivity for all tests conducted at piezometers screened in the Eocene units (i.e., all piezometers except for B-114A).

The calculation of hydraulic conductivity and transmissivity values from the slug test data generated from each piezometer was performed using equations pertinent for groundwater-bearing units under confined conditions, with the exception of the data generated from piezometer B-114A, which was determined to be under unconfined conditions. A determination of whether a piezometer was under confined or unconfined conditions was based on a review of the lithologic data in the boring logs and piezometer construction logs. An anisotropy ratio (K_v/K_h) of 0.1 was used in the calculation of the hydraulic conductivity and transmissivity values. It has long been established (consensus opinion) that horizontally bedded and/or stratified sedimentary deposits – such as the Eocene – have significant anisotropy and a permeability anisotropy of (K_v/K_h) of 0.1 was assumed as a conservative upper limit. Note that the *Yegua-Jackson Groundwater Availability Model* (TWDB, 2010) used 0.01 or less.

Hydraulic conductivity values calculated using the Hvorslev method were determined using Hvorslev Method F as this method was most appropriate based on subsurface conditions and the piezometer construction. Method F is for a well-screen under approximately confined conditions, etc. Also, for the available well-screen method choices, Method F will be the most conservative for estimating permeability. The filter pack length was used in the calculations in

place of the actual screened interval due to the significant difference between the hydraulic conductivity of the filter pack and the surrounding formation.

The AQTESOLV™ results showed a significant range in estimated hydraulic conductivity for the eight piezometers screened in the confined Eocene units. Hydraulic conductivity values determined using the Bouwer-Rice method ranged from 1.9×10^{-8} centimeters per second (cm/sec) in B-11A to 1.7×10^{-5} cm/sec in B-126. Hydraulic conductivity values determined using the Hvorslev method ranged from 2.9×10^{-8} cm/sec in B-11A to 2.5×10^{-5} cm/sec in B-126. Using the Cooper, et al method, hydraulic conductivity values ranged from 5.8×10^{-10} cm/sec in B-115 to 5.2×10^{-5} cm/sec in B-126; and transmissivity values ranged from 2.7×10^{-7} cm²/sec in B-115 to 3.8×10^{-2} cm²/sec in B-126.

Hydraulic conductivity values determined for the piezometer screened in the shallow alluvium (B-114A; unconfined hydrogeologic conditions) ranged from 1.5×10^{-7} cm/sec to 1.7×10^{-5} cm/sec using the Bouwer-Rice method and 2.0×10^{-7} cm/sec to 2.4×10^{-5} cm/sec using the Hvorslev method.

AQTESOLV™ results were confirmed by separate analyses. Semi-log plots of drawdown versus log time were manually prepared for multiple tests from piezometers B-102, B-106, B-114A, B-118, and B-126. The resulting plots had a typical “S-curve” signature. Plots showed data could be reasonably analyzed using “straight-line” solution methods, e.g., Hvorslev, applied to the mid-section of the signature and/or curve-matching using the Cooper, Bredehoeft & Papadopoulos Method (1967) [or Papadopoulos, Bredehoeft, and Cooper Method (1973)]. More importantly, the plots conclusively showed that the later time-drawdown data was representative of the formation – at least in near proximity to the borehole.

The highest hydraulic conductivity and transmissivity values were observed in piezometers B-126 (lower 10^{-5} cm/sec range) and B-102 (upper 10^{-6} to lower 10^{-5} cm/sec range). The lowest hydraulic conductivity and transmissivity values were observed in piezometers B-11A, B-109A, B-115, and B-118, all of which were in the upper 10^{-8} to lower 10^{-7} cm/sec range.

3.0 PUMP-DOWN TESTS

Pump-down tests on piezometers B-101, B-102, B-114A, B-124, and B-126 were conducted between April 2, 2012 and April 5, 2012. The rationale for conducting pump-down tests was to place maximum stress on the potentially transmissive unit by completely evacuating water from the piezometers (to the extent possible allowed by the submersible pump). The water-level recovery of these piezometers was then analyzed to determine hydrogeologic parameters.

3.1 Setup

Prior to conducting each pump-down test, a pressure transducer was programmed using a laptop computer. The date, time, site information, and logging instructions were programmed. The logging instructions consisted of recording the date, actual time, elapsed time, barometric pressure, water pressure, and the level of the water column over the pressure transducer (in feet).

In addition, the sample frequency/schedule of the transducer was configured to record data at one-minute (60 second) intervals. The submersible pump was placed approximately one foot above the bottom of the piezometer. The pressure transducer was then placed in the piezometer approximately two feet above the top of the submersible pump. Note that, as a consequence of transducer placement, early recovery data could not be obtained. This was not considered a significant problem because (1) the complete time-drawdown signature could be inferred and (2) the relatively linear middle portion of the time-drawdown data was actually used for analyses. The transducer cable was secured at the top of the piezometer so that the pressure transducer level in the piezometer was not altered during the test. Any transducer cable extruding out of the piezometer was placed away from areas of walking or vehicle traffic.

The static water level in the piezometer was measured with both the pressure transducer and a water level meter to confirm the transducer was functioning properly. In addition, the hydrostatic pressure at the transducer elevation was calculated and compared to the pressure measured by the transducer.

3.2 Pump-Down Recovery Test

Following confirmation that the transducer was functioning properly, the pump was activated to purge groundwater from the piezometer to a level below the pump. The decreasing head of the

water column was monitored by the field personnel with a laptop computer. Once the groundwater was purged to a level below the pump, the pump was allowed to run for approximately two to three minutes to ensure no late-time influx of groundwater flowed into the piezometer. Following this period of time the pump was then shut off and left in place while groundwater recovered into the piezometer.

The recovery test was considered complete when the water level had recovered to within ten percent of the original pre-pumping water levels or when at least 24 hours had elapsed since the pump was deactivated. Due to the very slow recovery of groundwater in piezometers B-114A and B-124, only one pump-down test was performed.

3.3 Pump-Down Data Evaluation and Results

The recovery data was first evaluated by plotting recovery (i.e., head) with respect to time. This pre-analysis processing step was performed to determine whether the transducer was properly measuring and recording recovery. A review of the recovery curves with respect to time determined the recovery data was usable and was ready for hydrogeologic evaluation.

Hydraulic conductivity was determined for each recovery test using Hvorslev Method F as this method was most appropriate based on the subsurface conditions and the piezometer construction. Based on the curvature present in the recovery data from the slug tests, pump-down recovery data was also analyzed using Cooper, et al method to determine transmissivity. The hydrogeologic conditions (i.e., confined or unconfined) and piezometer construction parameters (i.e., filter pack length used for screen length, etc.) used to calculate hydraulic conductivity/transmissivity from the slug test data was used in the calculation of the pump-down recovery data. Additional details necessary for the calculations, such as piezometer construction details, are provided in the attached Table 2.

Hydraulic conductivity values calculated using the Hvorslev method for the piezometers screened in the confined Eocene sand units showed a range of hydraulic conductivity values that ranged approximately two orders of magnitude. Hydraulic conductivity values calculated from tests conducted at piezometer B-101 ranged from 4.75×10^{-6} cm/sec to 3.87×10^{-6} cm/sec. Hydraulic conductivity values calculated from tests conducted on B-102 ranged from 1.11×10^{-5} cm/sec to 1.09×10^{-5} cm/sec. Hydraulic conductivity calculated from the test performed on B-

124 was 6.18×10^{-7} cm/sec. Hydraulic conductivity calculated from tests performed on B-126 ranged from 7.59×10^{-6} cm/sec to 4.95×10^{-6} cm/sec.

The hydraulic conductivity value determined for the piezometer screened in the shallow alluvium (B-114A; unconfined hydrogeologic conditions) was calculated to be 6.58×10^{-7} cm/sec.

Analysis of the recovery data for all five piezometers was attempted using the Cooper, *et al* method; however, none of the field recovery curves matched to the Cooper, *et al* method function curves, with the exception of the data collected from B-124. Since the recovery curves generated from tests conducted on piezometers B-101, B-102, B-114A, and B-126 did not match the Cooper-type function curves; this method was determined not to be appropriate. The transmissivity calculated from the data generated from the test on B-124 was 2.05×10^{-3} cm²/sec. Using the saturated thickness parameters provided in Table 2, the hydraulic conductivity calculated using the Cooper, *et al* method was 4.50×10^{-6} cm/sec.

AQTESOLV™ results were confirmed by separate analyses. Semi-log plots of drawdown versus log time were manually prepared for piezometers B-101, B-102, B-114A, B-124, and B-126 and the “straight-line” portion of the time-drawdown signature was analyzed using Hvorslev Method F.

4.0 SUMMARY AND CONCLUSIONS

Note that analytical results obtained at a given piezometer using all three methods, Bouwer-Rice, Hvorslev, and Cooper *et al*, were comparable as illustrated in Tables 1 and 2. The results also show that testing of what was assumed to be the most transmissive units in the subsurface showed that those units weren't very transmissive. To put the results in perspective, it is instructive to compare the obtained results to a common classification system illustrated below:

Permeability and Drainage Characteristics of Soils

Original reference: *Soil Mechanics in Engineering Practice*, Terzaghi and Peck, 1948 (based on earlier work, *Notes on Soil Testing for Engineering Purposes*, Casagrande and Fadum, 1940). Widely published since in various textbooks and reference books.

| | | | | | | | | | | | | |
|----------------------------------|---------------------------|---------------------------|---------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|-------------------------------|----------------------------|----------------------------|----------------------------|
| k, cm/sec (log scale) | <10² | <10¹ | <10⁰ | <10⁻¹ | <10⁻² | <10⁻³ | <10⁻⁴ | <10⁻⁵ | <10⁻⁶ | <10⁻⁷ | <10⁻⁸ | <10⁻⁹ |
| Drainage | Good | | | | | | Poor | | Practically Impervious | | | |

Based on the system shown above, the test results would all fall in the poorly permeable to practically impervious range.

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Bouwer, Herman & R.C. Rice, “A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers With Completely or Partially Penetrating Wells,” *Water Resources Research*, Volume 12, Number 3, American Geophysical Union, 1976.

Cooper, H.H., Bredehoeft, J.D., & Papadopoulos, I.S., “Response of a finite-diameter well to an instantaneous change of water,” *Water Resources Research*, Volume 3, Number 1, American Geophysical Union, 1967.

Deeds, Neil E. et al, *Groundwater Availability Model for the Yegua-Jackson Aquifer, Final Report*, Texas Water Development Board, March 2010.

Hvorslev, M. Juul, *Time Lag and Soil Permeability in Ground-Water Observations*, Bulletin 36, Waterways Experiment Station, U.S. Army Corps of Engineers, Vicksburg, Mississippi, 1951.

Papadopoulos, I.S., Bredehoeft, J.D., & Cooper, H.H., “On the analysis of ‘slug test’ data,” *Water Resources Research*, Volume 9, Number 1, American Geophysical Union, 1973.

TABLES

TABLE 1 - PIEZOMETER SLUG TEST RESULTS
Rancho Viejo Cattle Co.
Laredo, TX

Technically Complete, March 11, 2016

Appendix III-E.4

| Piezometer ID | Test | Date | Depth to Water (ft btoc) | Total Depth (ft btoc) | Duration (hrs) | h _i /H _i Recovery (%) | Time-Drawdown Response (log h _i /H _i vs. time) | Slug Length (ft) | Calculated Slug Volume Displacement s(0) (ft) | AQTESOLV INPUTS | | | | | | | | | | AQTESOLV RESULTS | | | | | |
|---|----------------|-----------|--------------------------|-----------------------|----------------|---|--|------------------|---|---------------------------------|----------------------------|----------------------------|---------------------------|--------------------------------------|--|--------------------------|---------------------------|-----------------------------|-----------------------------------|------------------|-------------------------------|----------------------------|--------------------------------|------------------|------------------|
| | | | | | | | | | | Observed Displacement s(0) (ft) | Static Water Column H (ft) | Saturated Thickness D (ft) | Filter Pack Length L (ft) | Well Screen Penetration Depth H (ft) | Anisotropy Ratio k _v /k _h -- | Casing Radius r (c) (ft) | Wellbore Radius r(w) (ft) | Well Skin Radius r(sk) (ft) | Effective Porosity Sand Pack n -- | Aquifer Model | Bouwer-Rice Method K (cm/sec) | Hvorslev Method K (cm/sec) | Cooper-Bredehoeft-Papadopoulos | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | |
| B-11A (Sands in Eocene using Sonic) | Slug In 1 | 1/12/2012 | 4.41 | 107.97 | 19.53 | 26.9% | Straight Line | 8 | 3.320 | -2.246 | 103.56 | 12 | 12 | 12 | 0.1 | 0.083 | 0.25 | 0.25 | 0.3 | Confined | 1.123E-07 | 1.732E-07 | 1.982E-07 | 7.250E-05 | 3.364E-06 |
| | Slug Out 1 | 1/13/2012 | 2.5 | | 24.42 | 7.4% | Straight Line | 8 | 3.320 | 2.327 | 105.47 | | | | | | | | | | 1.923E-08 | 2.964E-08 | 1.461E-09 | 5.343E-07 | 1.522E-02 |
| | Slug In 2 | 1/14/2012 | 4.66 | | 21.81 | 29% | Straight Line | 4 | 1.660 | -1.138 | 103.31 | | | | | | | | | | 1.150E-07 | 1.755E-07 | 2.128E-07 | 7.784E-05 | 3.007E-06 |
| | Slug Out 2 | 1/15/2012 | 3.89 | | 25.22 | 21.1% | Straight Line | 4 | 1.660 | 1.190 | 104.08 | | | | | | | | | | 5.958E-08 | 9.184E-08 | 3.278E-08 | 1.199E-05 | 1.648E-03 |
| | Slug In 3 | 1/16/2012 | 4.82 | | 6.59 | 8.1% | Straight Line | 8 | 3.320 | -2.245 | 103.15 | | | | | | | | | | 8.284E-08 | 1.277E-07 | 3.800E-08 | 1.390E-05 | 8.009E-04 |
| | Slug Out 3 | 1/17/2012 | 3.01 | | 25.05 | 13.8% | Straight Line | 8 | 3.320 | 2.328 | 104.96 | | | | | | | | | | 3.823E-08 | 5.893E-08 | 2.271E-08 | 8.305E-06 | 7.286E-04 |
| Average | | | | | | | | | | | | | | | | | | | | | 6.004E-08 | 9.241E-08 | 3.469E-08 | 1.269E-05 | 2.300E-04 |
| B-101 (Sands in Eocene using GPI) | Slug In 1 | 1/12/2012 | 7.69 | 92.75 | 4.27 | 87.5% | Straight Line | 8 | 3.320 | -2.264 | 85.06 | 14 | 14 | 14 | 0.1 | 0.083 | 0.25 | 0.25 | 0.3 | Confined | 3.097E-06 | 4.734E-06 | 5.896E-06 | 2.516E-03 | 1.000E-05 |
| | Slug Out 1 | 1/12/2012 | 7.23 | | 17.31 | 78.0% | Concave Up | 8 | 3.320 | 2.359 | 85.52 | | | | | | | | | | 4.050E-08 | 6.658E-08 | 1.790E-06 | 7.639E-04 | 8.000E-04 |
| | Slug In 2 | 1/13/2012 | 7.75 | | 21.46 | 93.3% | Concave Up | 12 | 4.980 | -3.367 | 85.00 | | | | | | | | | | 2.921E-07 | 4.724E-07 | 2.522E-06 | 1.076E-03 | 8.056E-04 |
| | Slug Out 2 | 1/14/2012 | 7.51 | | 4.46 | 82.8% | Concave Up | 12 | 4.980 | 3.514 | 85.24 | | | | | | | | | | 2.057E-06 | 3.107E-06 | 3.724E-06 | 1.589E-03 | 1.598E-04 |
| | Slug In 3 | 1/14/2012 | 8.10 | | 19.84 | 76.5% | Concave Up | 8 | 3.320 | -2.246 | 84.65 | | | | | | | | | | 7.439E-08 | 1.086E-07 | 2.578E-06 | 1.100E-03 | 1.500E-04 |
| | Slug Out 3 | 1/15/2012 | 7.49 | | 3.35 | 75.7% | Concave Up | 8 | 3.320 | 2.353 | 85.26 | | | | | | | | | | 2.254E-06 | 3.406E-06 | 3.890E-06 | 1.660E-03 | 1.211E-04 |
| Average | | | | | | | | | | | | | | | | | | | | | 4.826E-07 | 7.451E-07 | 3.159E-06 | 1.348E-03 | 1.629E-04 |
| B-102 (Sands in Eocene using GPI) | Slug In 1 | 1/12/2012 | 8.65 | 62.82 | 3.54 | 100% | Straight Line | 10 | 4.150 | -2.868 | 54.17 | 14 | 14 | 14 | 0.1 | 0.083 | 0.25 | 0.25 | 0.3 | Confined | 1.034E-05 | 1.580E-05 | 3.180E-05 | 1.357E-02 | 2.158E-08 |
| | Slug Out 1 | 1/12/2012 | 8.66 | | 8.87 | 96.2% | Concave Up | 10 | 4.150 | 2.899 | 54.16 | | | | | | | | | | 6.479E-06 | 9.820E-06 | 1.250E-05 | 5.336E-03 | 3.359E-04 |
| | Slug In 2 | 1/13/2012 | 8.76 | | 2.78 | 94.6% | Concave Up | 13 | 5.395 | -4.092 | 54.06 | | | | | | | | | | 5.735E-06 | 8.691E-06 | 1.011E-05 | 4.313E-03 | 1.180E-03 |
| | Slug Out 2 | 1/13/2012 | 8.60 | | 1.43 | 84.5% | Concave Up | 13 | 5.395 | 3.876 | 54.22 | | | | | | | | | | 6.345E-06 | 9.621E-06 | 1.634E-05 | 6.971E-03 | 2.572E-05 |
| | Slug In 3 | 1/14/2012 | 8.90 | | 1.70 | 94.7% | Straight Line | 15 | 6.225 | -4.293 | 53.92 | | | | | | | | | | 1.041E-05 | 1.593E-05 | 1.913E-05 | 8.164E-03 | 1.011E-05 |
| | Slug Out 3 | 1/14/2012 | 8.36 | | 1.12 | 77.3% | Concave Up | 15 | 6.225 | 4.307 | 54.46 | | | | | | | | | | 5.920E-06 | 8.973E-06 | 1.195E-05 | 5.101E-03 | 2.642E-04 |
| Average | | | | | | | | | | | | | | | | | | | | | 7.291E-06 | 1.108E-05 | 1.571E-05 | 6.703E-03 | 2.894E-05 |
| B-106 (Sands in Eocene using GPI) | Slug In 1 | 1/12/2012 | 7.60 | 83.16 | 3.95 | 78.0% | Concave Up | 10 | 4.150 | -2.789 | 75.56 | 14 | 14 | 14 | 0.1 | 0.083 | 0.25 | 0.25 | 0.3 | Confined | 2.083E-06 | 3.205E-06 | 3.433E-06 | 1.465E-04 | 1.889E-04 |
| | Slug Out 1 | 1/13/2012 | 7.55 | | 5.93 | 73.3% | Concave Up | 10 | 4.150 | 2.938 | 75.61 | | | | | | | | | | 9.112E-07 | 1.358E-06 | 1.198E-06 | 5.110E-04 | 3.499E-03 |
| | Slug In 2 | 1/13/2012 | 8.29 | | 4.53 | 65.9% | Concave Up | 13 | 5.395 | -3.664 | 74.87 | | | | | | | | | | 8.246E-07 | 1.246E-06 | 1.111E-06 | 4.741E-04 | 4.680E-03 |
| | Slug Out 2 | 1/14/2012 | 7.58 | | 4.53 | 69.0% | Concave Up | 13 | 5.395 | 3.909 | 75.58 | | | | | | | | | | 1.141E-06 | 1.738E-06 | 1.308E-06 | 5.580E-04 | 3.307E-03 |
| | Slug In 3 | 1/14/2012 | 8.44 | | 16.70 | 74.2% | Concave Up | 10 | 4.150 | -2.854 | 74.72 | | | | | | | | | | 7.290E-08 | 1.116E-07 | 9.257E-07 | 3.950E-04 | 6.095E-03 |
| | Slug Out 3 | 1/15/2012 | 7.67 | | 4.73 | 71.7% | Concave Up | 10 | 4.150 | 2.934 | 75.49 | | | | | | | | | | 1.149E-06 | 1.746E-06 | 1.534E-06 | 6.544E-04 | 2.226E-03 |
| Average | | | | | | | | | | | | | | | | | | | | | 7.286E-07 | 1.107E-06 | 1.428E-06 | 6.094E-04 | 2.275E-03 |
| B-109A (Sands in Eocene using Sonic) | Slug In 2 | 1/14/2012 | 6.71 | 83.99 | 16.81 | 29.5% | Straight Line | 8 | 3.320 | -2.320 | 86.04 | 12 | 12 | 12 | 0.1 | 0.083 | 0.25 | 0.25 | 0.3 | Confined | 1.389E-07 | 2.142E-07 | 9.900E-08 | 3.621E-05 | 8.920E-04 |
| | Slug Out 2 | 1/15/2012 | 4.78 | | 24.08 | 11.9% | Straight Line | 8 | 3.320 | 2.342 | 87.97 | | | | | | | | | | 3.409E-08 | 5.255E-08 | 1.839E-08 | 6.726E-06 | 8.444E-04 |
| | Slug In 3 | 1/16/2012 | 6.88 | | 23.20 | 27.8% | Straight Line | 8 | 3.320 | -2.250 | 85.87 | | | | | | | | | | 9.978E-08 | 1.538E-07 | 1.965E-07 | 7.189E-05 | 1.156E-06 |
| | Slug Out 3 | 1/17/2012 | 5.23 | | 22.69 | 16.5% | Straight Line | 8 | 3.320 | 2.395 | 87.52 | | | | | | | | | | 4.839E-08 | 7.458E-08 | 1.150E-08 | 4.205E-06 | 6.806E-03 |
| | Average | | | | | | | | | | | | | | | | | | | | | 6.915E-08 | 1.066E-07 | 4.504E-08 | 1.647E-05 |
| B-114A (Shallow Alluvium; Eocene-Quaternary Contact?) | Slug In 1 | 1/12/2012 | 10.24 | 22.78 | 2.47 | 61.8% | Concave Up | 3 | 1.245 | -0.783 | 12.54 | 10 | 10 | 10 | 0.1 | 0.083 | 0.25 | 0.25 | 0.3 | Unconfined | 3.743E-06 | 4.969E-06 | -- | -- | -- |
| | Slug Out 1 | 1/12/2012 | 9.72 | | 18.97 | 37.5% | Concave Up | 3 | 1.245 | 0.843 | 13.06 | | | | | | | | | | 1.448E-07 | 2.046E-07 | -- | -- | -- |
| | Slug In 2 | 1/13/2012 | 10.28 | | 2.06 | 52.8% | Concave Up | 5 | 2.075 | -1.310 | 12.50 | | | | | | | | | | 2.546E-06 | 3.649E-06 | -- | -- | -- |
| | Slug Out 2 | 1/13/2012 | 9.68 | | 1.60 | 15.1% | Straight Line | 5 | 2.075 | 1.321 | 13.10 | | | | | | | | | | 1.013E-06 | 1.423E-06 | -- | -- | -- |
| | Slug In 3 | 1/13/2012 | 10.78 | | 18.02 | 54.4% | Concave Up | 5 | 2.075 | -1.259 | 12.00 | | | | | | | | | | 1.457E-07 | 2.071E-07 | -- | -- | -- |
| | Slug Out 3 | 1/14/2012 | 10.18 | | 1.84 | 32.6% | Straight Line | 5 | 2.075 | 1.329 | 12.60 | | | | | | | | | | 2.306E-06 | 3.284E-06 | -- | -- | -- |
| | Slug In 4 | 1/17/2012 | 10.24 | | 16.27 | 100% | Straight Line | 5 | 2.075 | -1.326 | 12.54 | | | | | | | | | | 1.670E-05 | 2.361E-05 | -- | -- | -- |
| | Slug Out 4 | 1/18/2012 | 10.25 | | 21.06 | 94.1% | Straight Line | 5 | 2.075 | 1.327 | 12.53 | | | | | | | | | | 1.541E-06 | 2.197E-06 | -- | -- | -- |
| Average | | | | | | | | | | | | | | | | | | | | | 1.365E-06 | 1.922E-06 | -- | -- | -- |
| B-115 (Sands in Eocene using Sonic) | Slug In 1 | 1/15/2012 | 7.16 | 104.48 | 22.65 | 66.3% | Concave Up | 10 | 4.150 | -2.790 | 97.32 | 15 | 15 | 15 | 0.1 | 0.083 | 0.25 | 0.25 | 0.3 | Confined | 2.209E-07 | 3.357E-07 | 3.073E-07 | 1.405E-04 | 6.315E-04 |
| | Slug Out 1 | 1/16/2012 | 5.92 | | 8.43 | 7.4% | Straight Line | 10 | 4.150 | 2.888 | 98.56 | | | | | | | | | | 3.333E-08 | 5.082E-08 | 5.822E-10 | 2.662E-07 | 1.000E-01 |
| | Slug In 2 | 1/16/2012 | 8.64 | | 15.35 | 20.8% | Straight Line | 10 | 4.150 | -2.795 | 95.84 | | | | | | | | | | 4.601E-08 | 6.343E-08 | 2.421E-09 | 1.107E-06 | 1.000E-01 |
| | Slug Out 2 | 1/17/2012 | 6.35 | | 25.18 | 39.8% | Concave Up | 10 | 4.150 | 2.918 | 98.13 | | | | | | | | | | 3.567E-08 | 5.439E-08 | 8.248E-08 | 3.771E-05 | 3.199E-02 |
| | Average | | | | | | | | | | | | | | | | | | | | | 5.896E-08 | 8.759E-08 | 1.375E-08 | 6.286E-06 |
| B-118 (Silt in Eocene using Sonic) | Slug In 2 | 1/14/2012 | 11.95 | 87.55 | 15.59 | 82.9% | Concave Up | 15 | 6.225 | -4.160 | 75.60 | 12 | 12 | 12 | 0.10 | 0.083 | 0.25 | 0.25 | 0.3 | Confined | 7.170E-07 | 1.096E-06 | 1.335E-06 | 4.883E-04 | 6.667E-05 |
| | Slug Out 2 | 1/15/2012 | 11.06 | | 25.82 | 76.3% | Concave Up | 15 | 6.225 | 4.330 | 76.49 | | | | | | | | | | 1.616E-07 | 2.373E-07 | 4.273E-07 | 1.563E-04 | 2.784E-03 |
| | Slug In 3 | 1/16/2012 | 12.14 | | 20.48 | 81.5% | Concave Up | 15 | 6.225 | -4.138 | 75.41 | | | | | | | | | | 4.076E-07 | 6.236E-07 | 8.257E-07 | 3.020E-04 | 4.570E-04 |
| | Slug Out 3 | 1/17/2012 | 11.31 | | 24.21 | 79.2% | Concave Up | 15 | 6.225 | 4.326 | 76.24 | | | | | | | | | | 1.874E-07 | 2.819E-07 | 5.982E-07 | 2.188E-04 | 1.120E-03 |
| | Slug In 4 | 1/18/2012 | 12.25 | | 8.78 | 56.0% | Concave Up | 10 | 4.150 | -2.755 | 75.30 | | | | | | | | | | 4.954E-07 | 7.597E-07 | 6.644E-07 | 2.430E-04 | 6.638E-04 |
| | Slug Out 4 | 1/18/2012 | 11.11 | | 14.85 | 60.1% | Concave Up | 10 | 4.150 | 2.933 | 76.44 | | | | | | | | | | 2.325E-07 | 3.311E-07 | 3.284E-07 | 1.201E-04 | 3.342E-03 |
| Average | | | | | | | | | | | | | | | | | | | | | 3.172E-07 | 4.751E-07 | 6.282E-07 | 2.298E-04 | 7.714E-04 |
| B-126 (Sands in Eocene using Sonic) | Slug In 1 | 1/13/2012 | 8.58 | 105.55 | 4.53 | 100% | Straight Line | 10 | 4.150 | -2.920 | 96.97 | 24 | 24 | 24 | 0.1 | 0.083 | 0.25 | 0.25 | 0.3 | Confined | 1.645E-05 | 2.467E-05 | 5.165E-05 | 3.778E-02 | 7.213E-09 |
| | Slug Out 1 | 1/14/2012 | 8.47 | | 2.78 | 99.2% | Concave Up | 10 | 4.150 | 2.913 | 97.08 | | | | | | | | | | 1.236E-05 | 1.833E-05 | 2.524E-05 | 1.846E-02 | 2.570E-06 |
| | Slug In 2 | 1/14/2012 | 8.50 | | 1.56 | 97.3% | Concave Up | 13 | 5.395 | -3.754 | 97.05 | | | | | | | | | | 1.396E-05 | 2.088E-05 | 3.498E-05 | 2.559E-02 | 1.144E-06 |
| | Slug Out 2 | 1/14/2012 | 8.46 | | 1.32 | 97.2% | Concave Up | 13 | 5.395 | 3.898 | 97.09 | | | | | | | | | | 1.439E-05 | 2.155E-05 | 3.143E-05 | 2.299E-02 | 1.012E-06 |
| | Slug In 3 | 1/14/2012 | 8.55 | | 0.88 | 94.6% | Concave Up | 13 | 5.395 | -3.668 | 97.00 | | | | | | | | | | 1.419E- | | | | |

TABLE 2 - PIEZOMETER PUMP DOWN TEST RESULTS
Pescadito Environmental Resource Center
Laredo, TX

Technically Complete, March 11, 2016

Appendix III-E.4

| Piezometer ID | Test | Date | Depth to Water * (ft btoc) | Total Depth (ft btoc) | Duration (hrs) | Recovery (%) | Approximate Volume Purged (Gal) | Drawdown relative to static water level at Time 1 | Drawdown relative to static water level at Time 2 | Time 2 | Saturated Thickness (ft) | Filter Pack Length (ft) | Anisotropy Ratio k_v/k_h | Piezometer Casing Diameter (ft) | Borehole/Filter Pack Diameter (ft) | Transformation Ratio $(K_v/K_h)^{1/2}$ | GWBU Condition | Hvorslev Method | Cooper-Bredehoeft-Papadopulos | | |
|---|--------------------|----------|----------------------------|-----------------------|----------------|--------------|---------------------------------|---|---|----------------------|--------------------------|-------------------------|----------------------------|---------------------------------|------------------------------------|--|----------------|------------------|-------------------------------|------------|------------|
| | | | | | | | | H ₁ (ft) | H ₂ (ft) | t ₂ (sec) | | | | | | | | D (ft) | L (ft) | r (c) (ft) | r (w) (ft) |
| B-101 (Sands in Eocene using GPI) | Test 04/03 - 04/04 | 4/3/2012 | 3.09 | 92.85 | 22.96 | 94.6% | 17.25 | 39.494 | 6900.000 | 64.031 | 15420.000 | 4.5 | 14 | 0.1 | 0.167 | 0.5 | 3.162 | Confined | 3.874E-06 | -- | -- |
| | Test 04/04 - 04/05 | 4/4/2012 | 9.29 | | 21.10 | 99.4% | 14 | 27.414 | 4140.000 | 54.176 | 10500.000 | | | | | | | | 4.737E-06 | -- | -- |
| Average | | | | | | | | | | | | | | | | | | 4.283E-06 | -- | -- | |
| B-102 (Sands in Eocene using GPI) | Test 04/03 - 04/04 | 4/3/2012 | 6.1 | 63.05 | 21.46 | 94.5% | 14 | 14.958 | 2160.000 | 36.018 | 5400.000 | 9 | 14 | 0.1 | 0.167 | 0.5 | 3.162 | Confined | 1.115E-05 | -- | -- |
| | Test 04/04 - 04/05 | 4/4/2012 | 9.38 | | 21.68 | 99.4% | 8.5 | 15.034 | 2100.000 | 30.048 | 4380.000 | | | | | | | | 1.096E-05 | -- | -- |
| Average | | | | | | | | | | | | | | | | | | 1.105E-05 | -- | -- | |
| B-114A (Shallow Alluvium; Eocene-Quaternary Contact?) | Test 04/02 - 04/04 | 4/2/2012 | 9.55 | 22.97 | 52.08 | 79.6% | 4.5 | 2.939 | 108720.000 | 6.037 | 151260.000 | 12.54 | 12 | 0.1 | 0.167 | 0.5 | 3.162 | Unconfined | 6.58722E-07 | -- | -- |
| B-124 (Sands in Eocene using Sonic) | Test 04/02 - 04/04 | 4/2/2012 | 1.9 | 117.2 | 62.88 | 92.1% | 18.75 | 40.211 | 20940.000 | 80.89 | 78060 | 15 | 15 | 0.1 | 0.167 | 0.5 | 3.162 | Confined | 6.168E-07 | 4.501E-06 | 2.058E-03 |
| B-126 (Sands in Eocene using Sonic) | Test 04/03 - 04/04 | 4/3/2012 | 4.05 | 104.31 | 25.16 | 97.5% | 22.5 | 30.640 | 4200.000 | 74.91 | 10320.00 | 24 | 24 | 0.1 | 0.167 | 0.5 | 3.162 | Confined | 7.598E-06 | -- | -- |
| | Test 04/05 - 04/06 | 4/5/2012 | 3.04 | | 19.16 | 93.6% | 18 | 42.594 | 5820.000 | 76.30 | 13800.00 | | | | | | | | 4.957E-06 | -- | -- |
| Average | | | | | | | | | | | | | | | | | | 6.137E-06 | -- | -- | |

NOTES

* - Measured with equipment in the piezometer

ASSUMPTIONS

Filter pack interval will be used as the screen length during slug test analyses due to the relative difference between typical filter pack permeability and expected formation permeability